Campus: UCLA Building Name: Transit Operations Center CAAN ID: 4522 Auxiliary Building ID:



UNIVERSITY OF CALIFORNIA

Date: Feb 17, 2021

## FORM 1 CERTIFICATE OF SEISMIC PERFORMANCE LEVEL UC-Designed & Constructed Facility Campus-Acquired or Leased Facility

#### **BUILDING DATA**

Building Name: Transit Operations Center Address: 11075 Kinross Ave Los Angeles, CA 90024 Site location coordinates: Latitude 34.0594893 Longitudinal -118.4483786

#### UCOP SEISMIC PERFORMANCE LEVEL (OR "RATING"): V

ASCE 41-17 Model Building Type:

- a. Longitudinal Direction: No Model Building Type (Manufactured Housing)
- b. Transverse Direction: No Model Building Type (Manufactured Housing)

Gross Square Footage: 3,456 Number of stories *above* grade: 1 Number of basement stories *below* grade: 0

Year Original Building was Constructed: 2004 Original Building Design Code & Year: CBC-2001 Retrofit Building Design Code & Code (if applicable): N/A

#### SITE INFORMATION

Site Class: D	Basis:	Inferred
Geologic Hazards:		
Fault Rupture: No	Basis:	CGS Earthquake Hazards Zone Application
Liquefaction: Yes	Basis:	CGS Earthquake Hazards Zone Application
Landslide: No	Basis:	CGS Earthquake Hazards Zone Application

#### ATTACHMENT

Original Structural Drawings: (N/A, N/A, N/A, N/A) or
 Seismic Evaluation: (Transit Operations Center Seismic Evaluation, KPFF, 2/17/2021, FEMA 154 Rapid Visual Screening)
 Retrofit Structural Drawings: (N/A, N/A, N/A, N/A)



Date: Feb 17, 2021

#### **CERTIFICATION & PRESUMPTIVE RATING VERIFICATION STATEMENT**

I, Mark Hershberg, a California-licensed structural engineer, am responsible for the completion of this certificate, and I have no ownership interest in the property identified above. My scope of review to support the completion of this certificate included both of the following ("No" responses must include an explanation):

OF

UNIVERSITY

CALIFORNIA

- a) the review of structural drawings indicating that they are as-built or record drawings, or that they otherwise are the basis for the construction of the building: ☑ Yes □ No
- b) visiting the building to verify the observable existing conditions are reasonably consistent with those shown on the structural drawings: □ Yes ☑ No
   Due to COVID-19 protocols, observations were performed for exterior of building only.

Based on my review, I have verified that the UCOP Seismic Performance Level (SPL) is presumptively permitted by the following UC Seismic Program Guidebook provision (choose one of the following):

 $\Box$  1) Contract documents indicate that the original design and construction of the aforementioned building is in accordance with the benchmark design code year (or later) building code seismic design provisions for UBC or IBC listed in Table 1 below.

☑ 2) The existing SPL rating is based on an acceptable basis of seismic evaluation completed in 2006 or later.

□ 3) Contract documents indicate that a comprehensive<sup>1</sup> building seismic retrofit design was fullyconstructed with an engineered design based on the 1997 UBC/1998 *or later* CBC, and (choose one of the following):

□ the retrofit project was completed by the UC campus. Further, the design was based on ground motion parameters, at a minimum, corresponding to BSE-1E (or BSE-R) and BSE-2E (or BSE-C) as defined in ASCE 41, or the full design basis ground motion required in the 1997 UBC/1998 CBC *or later* for EXISTING buildings, and is presumptively assigned an SPL rating of IV.

□ the retrofit project was completed by the UC campus. Further, the design was based on ground motion parameters, at a minimum, corresponding to BSE-1 (or BSE-1N) and BSE-2 (or BSE-2N) as defined in ASCE 41, or the full design basis ground motion required in the 1997 UBC/1998 *or later* CBC for NEW buildings, and is presumptively assigned an SPL rating of III.

□ the retrofit project was not completed by the UC campus following UC policies, and is presumptively assigned an SPL rating of IV.

<sup>&</sup>lt;sup>1</sup> A comprehensive retrofit addresses the entire building structural system as indicated by the associated seismic evaluation, as opposed to addressing selective portions of the structural system.



# OF CALIFORNIA

Date: Feb 17, 2021

#### **CERTIFICATION SIGNATURE**

Mark Hershberg Print Name Principal Title

S5078

6/30/2021 License Expiration Date

CA Professional Registration No. Signature

2/17/2021

Date



AFFIX SEAL HERE

KPFF Inc., (213) 418-0201, 700 S. Flower St., Suite 2100, Los

Angeles, CA 90017

Firm Name, Phone Number, and Address

#### Table 1: Benchmark Building Codes and Standards

	Building Seismic Design Provisions					
Building Type <sup>a,b</sup>	UBC	IBC				
Wood frame, wood shear panels (Types W1 and W2)	1976	2000				
Wood frame, wood shear panels (Type W1a)	1976	2000				
Steel moment-resisting frame (Types S1 and S1a)	1997	2000				
Steel concentrically braced frame (Types S2 and S2a)	1997	2000				
Steel eccentrically braced frame (Types S2 and S2a)	1988 <sup>g</sup>	2000				
Buckling-restrained braced frame (Types S2 and S2a)	f	2006				
Metal building frames (Type S3)	f	2000				
Steel frame with concrete shear walls (Type S4)	1994	2000				
Steel frame with URM infill (Types S5 and S5a)	f	2000				
Steel plate shear wall (Type S6)	f	2006				
Cold-formed steel light-frame construction—shear wall system (Type CFS1)	1997 <sup>h</sup>	2000				
Cold-formed steel light-frame construction—strap-braced wall system (Type CFS2)	f	2003				
Reinforced concrete moment-resisting frame (Type C1) <sup>i</sup>	1994	2000				
Reinforced concrete shear walls (Types C2 and C2a)	1994	2000				
Concrete frame with URM infill (Types C3 and C3a)	f	f				
Tilt-up concrete (Types PC1 and PC1a)	1997	2000				
Precast concrete frame (Types PC2 and PC2a)	f	2000				
Reinforced masonry (Type RM1)	1997	2000				
Reinforced masonry (Type RM2)	1994	2000				
Unreinforced masonry (Type URM)	f	f				
Unreinforced masonry (Type URMa)	f	f				
Seismic isolation or passive dissipation	1991	2000				

Note: This table has been adapted from ASCE 41-17 Table 3-2. Benchmark Building Codes and Standards for Life Safety Structural Performed at BSE-1E. Note: UBC = Uniform Building Code. IBC = International Building Code.

<sup>a</sup> Building type refers to one of the common building types defined in Table 3-1 of ASCE 41-17.

<sup>b</sup> Buildings on hillside sites shall not be considered Benchmark Buildings.

<sup>c</sup> not used

<sup>d</sup> not used

<sup>e</sup> not used

<sup>f</sup> No benchmark year; buildings shall be evaluated in accordance with Section III.J.

<sup>g</sup> Steel eccentrically braced frames with links adjacent to columns shall comply with the 1994 UBC Emergency Provisions, published September/October 1994, or subsequent requirements.

 $^{\rm h}$  Cold-formed steel shear walls with wood structural panels only.

<sup>i</sup> Flat slab concrete moment frames shall not be considered Benchmark Buildings.



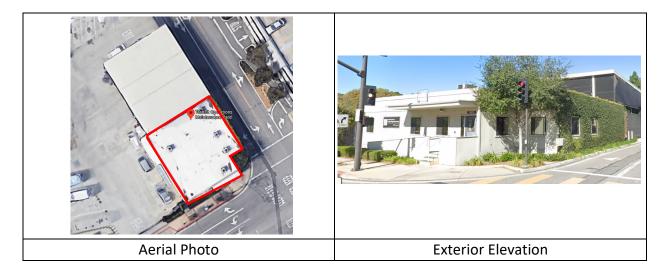
## UCLA – Transit Operations Center

DATE: 2/17/2021 ASCE 41-17 Tier 1 Seismic Evaluation Minimum Building Report Information

## **BUILDING DATA**

ROFESSION HERSAISH STATE STATE CALIFORNIA STATE STATE

Campus: UCLA Building Name: Transit Operations Center CAAN ID: 4522 Auxiliary Building ID: Address: 11075 Kinross Ave Los Angeles, CA 90024 Site location coordinates: Latitude 34.0594893 Longitudinal -118.4483786



ASCE 41-17 Model Building Type:

- a. Longitudinal Direction: No Model Building Type (Manufactured Housing)
- b. Transverse Direction: No Model Building Type (Manufactured Housing)

Site-specific Ground Motion Study? No

Seismic Design Acceleration Parameters of Interest:

- a. For BSE-1E  $S_{xs}=0.895g$  and  $S_{x1}=0.514g$
- b. For BSE-2E  $S_{XS}$ =1.541g and  $S_{X1}$ =0.943g

Estimated Fundamental Period (seconds)

- a. Longitudinal: Unknown
- b. Transverse: Unknown

Gross Square Footage: 3,456 Number of stories *above* grade: 1 Number of basement stories below grade: 0

Year Original Building was Constructed: 2004 Original Building Design Code & Year: CBC-2001 Retrofit Building Design Code & Code (if applicable): N/A

## SITE INFORMATION

Site Class: D	Basis:	Inferred
Geologic Hazards:		
Fault Rupture: No	Basis:	CGS Earthquake Hazards Zone Application
Liquefaction: Yes	Basis:	CGS Earthquake Hazards Zone Application
Landslide: No	Basis:	CGS Earthquake Hazards Zone Application

## UCOP SEISMIC PERFORMANCE RATING (OR "RATING"): V

## "BALLPARK" RETROFIT COST (if applicable)

- $\boxtimes$  Minor (<\$50/sf)
- □ Moderate (~\$50-\$200/sf)
- □ Major (>\$200/sf)

## SUMMARY TIER 1 SEISMIC EVALUATION STRUCTURAL NON-COMPLIANCES/FINDINGS SIGNIFICANTLY AFFECTING RATING DETERMINATION

Significant Structural Deficiencies, Potentially Affecting Seismic Performance Level Designation:

- Lateral System Stress Check (wall shear, column shear or flexure, or brace axial as applicable)
- Lateral System Detailing (reinforcement ratio, confinement, aspect ratio, etc)
- $\boxtimes$ Load Path
- **Adjacent Buildings**
- Weak Story
- Soft Story
- Geometry (vertical irregularities)
- Torsion
- Mass – Vertical Irregularity
- **Cripple Walls**
- Wood Sills (bolting)
- **Diaphragm Continuity**
- Openings at Shear Walls (concrete or masonry)
- $\boxtimes$ Liquefaction

Transit Operations Center – CAAN# 4522 UCLA Seismic Tier 1 Evaluation – Minimum Building Report Information

- Slope Failure
- Surface Fault Rupture
- Masonry or Concrete Wall Anchorage at Diaphragm
- URM wall height to thickness ratio
- **URM** Parapets or Cornices
- **URM Chimney**
- Heavy Partitions Braced by Ceilings
- Appendages

## POTENTIAL FALLING HAZARDS

- Heavy ceilings, features or ornamentation above large lecture halls, auditoriums, lobbies or other areas where large numbers of people congregate.
- Heavy masonry or stone veneer above exit ways.
- Unbraced masonry parapets, cornices or other ornamentation above exit ways.
- Unrestrained hazardous materials storage.
- Masonry chimneys.
- Unrestrained natural gas-fueled equipment such as water heaters, boilers, emergency generators, etc.
- $\boxtimes$ None of the above.

Due to current COVID-19 protocols, we did not verify in field that as-built documentation match current conditions or perform any condition assessment of the existing structure to identify falling hazards as required by the UCOP SSP.

## **BRIEF DESCRIPTION OF ANTICIPATED FAILURE MECHANISM**

Lack of anchorage which means that the building can potentially slide off of the foundation.

## COMMENTS AND RECOMMENDATIONS

Add anchorage to prevent building from sliding off foundation.

## Appendices

A. FEMA 154 Rapid Visual Screening

## Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

Other identifiers:       5-widde trailers         use:       Trainsit Operations Center         vs:       0.725         set:       0.726         vs:       0.727         vs: </th <th></th> <th colspan="9">Address: <u>11075 Kinross Ave.</u></th> <th></th>		Address: <u>11075 Kinross Ave.</u>																		
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## Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

#### Level 2 (Optional) VERY HIGH Seismicity

Optional Level 2 data collection to be performed by a civil or structural engineering professional, architect, or graduate student with background in seismic evaluation or design of buildings.

Bldg Name: Transit Ops CTR	Final Level 1 Score:	$S_{L1} = 1.6$	(do not consider $S_{MIN}$ )
Screener:	Level 1 Irregularity Modifiers:	Vertical Irregularity, $V_{L1}$ =	Plan Irregularity, $P_{L1}$ =
Date/Time:	ADJUSTED BASELINE SCORE:	$S' = (S_{L1} - V_{L1} - P_{L1}) =$	

STRUCTURA	L MODIFIE	RS TO ADD TO ADJUSTED BA	SELINE SCORE								
Topic	Statement (	If statement is true, circle the "Yes" mod					Yes	Subtotals			
Vertical	Sloping	W1 building: There is at least a full st	-0.9								
Irregularity, VL2	Site	Non-W1 building: There is at least a	full story grade change from one side of the building t	de of the building to the other0.2							
	Weak	W1 building cripple wall: An unbrace	d cripple wall is visible in the crawl space.				-0.5				
	and/or	W1 house over garage: Underneath	an occupied story, there is a garage opening without	a steel m	noment fr	ame,					
	Soft Story	and there is less than 8' of wall on the	e same line (for multiple occupied floors above, use 1	6' of wall	minimur	n).	-0.9				
	(circle one	W1A building open front: There are of	openings at the ground story (such as for parking) over	er at leas	t 50% of	the					
	maximum)	,									
		Non-W1 building: Length of lateral system at any story is less than 50% of that at story above or height of any									
		story is more than 2.0 times the heigh Non-W1 building: Length of lateral so	-0.7								
		eight									
	0.11.1	of any story is between 1.3 and 2.0 ti					-0.4				
	Setback		n at an upper story are outboard of those at the story	below ca	ausing th	е					
		diaphragm to cantilever at the offset.					-0.7				
			m at upper stories are inboard of those at lower storie				-0.4 -0.2				
	Short		ral elements that is greater than the length of the eler ast 20% of columns (or piers) along a column line in t		Lovetom	hava	10.2				
	Column/		the nominal height/depth ratio at that level.	ne latera	system	llave	-0.4				
	Pier		column depth (or pier width) is less than one half of th	ne denth	of the sn	andrel	10.4				
	1 101	or there are infill walls or adjacent flo				unuru,	-0.4				
	Split Level	There is a split level at one of the floor					-0.4	-			
	Other		vertical irregularity that obviously affects the building's	seismic	performa	ance.	-0.7	$V_{L2} = 0$			
	Irregularity		e vertical irregularity that may affect the building's se				-0.4	(Cap at -0.9)			
Plan	Torsional irre		ar relatively well distributed in plan in either or both di				/				
Irregularity, PL2	include the V	V1A open front irregularity listed above	)		•		-0.5/				
			vertical elements of the lateral system that are not orth			ther.	-0.2				
			corner exceed 25% of the overall plan dimension in t				-0/2				
			phragm with a width over 50% of the total diaphragm	width at	that leve	Ι.	-0.2	Ο			
			ams do not align with the columns in plan.				/-0.2	PL2 = 0			
			irregularity that obviously affects the building's seism	ic perfori	mance.		/-0.5	(Cap at -0.7)			
Redundancy			ts on each side of the building in each direction.				+0.2 /	No			
Pounding		eparated from an adjacent structure	The floors do not align vertically within 2 feet.		(Cap tota		-0.7	anchorage to			
		1.5% of the height of the shorter of	One building is 2 or more stories taller than the oth		poundin		-0.7	supporting			
00 D 11 I		and adjacent structure and:	The building is at the end of the block.		modifiers	at -0.9)	-0.4	curb			
S2 Building		eometry is visible.					-07	observed in			
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PC1/RM1 Bldg		nark or retrofit modifier.)	from drawings that do not rely on cross-grain bending	. ( <i>D0 110</i>		e with	+0.2	Investigation			
PC1/RM1 Bldg			walls (rather than an interior space with few walls suc	h as in a	warehou	160)	+0.2				
URM	Gable walls		wails (rather than an interior space with rew wails suc	11 43 111 4	warenot	130).	-0.3				
MH			ovided between the carriage and the ground.								
Retrofit		sive seismic retrofit is visible or known f						<sub>M=</sub> 0.0			
		$S_{L2} = (S' + V_{L2} + P_{L2} + M) \ge S_{MIN}$				(		to Level 1 form			
	ble damage or	$O_{L2} \rightarrow (O \rightarrow V_{L2} + F_{L2} + W) \geq O_{MA}$	I.O+O.O = I.O negatively affects the building's seismic performance:	ПY		No	nansiel				
			n the Level 1 form that detailed evaluation is required		_	-	a's score				
							, 00.0				
						r –	_				
Location	,	Check "Yes" or "No")		Yes	No		Com	ment			
Exterior			t or unbraced unreinforced masonry chimney.		/						
	There is hea	vy cladding or heavy veneer.		1	1 /	1					

Comments: