Campus: UCLA Building Name: Venice Dentistry CAAN ID: 4327 Auxiliary Building ID:



Date: Apr 27, 2021

## FORM 1 CERTIFICATE OF SEISMIC PERFORMANCE LEVEL

OF

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UC-Designed & Constructed Facility

**Campus-Acquired or Leased Facility** 

#### **BUILDING DATA**

Building Name: Venice Dentistry Address: 323 South Lincoln Blvd. Venice, CA 90291 Site location coordinates: Latitude 34.00096759 Longitudinal -118.4671674

#### UCOP SEISMIC PERFORMANCE LEVEL (OR "RATING"): V

ASCE 41-17 Model Building Type:

- a. Longitudinal Direction: W2: Wood frame, wood shear panels
- b. Transverse Direction: W2: Wood frame, wood shear panels

Gross Square Footage: 9,443 Number of stories *above* grade: 1 Number of basement stories *below* grade: 0

Year Original Building was Constructed: 1978 Original Building Design Code & Year: UBC-1973 Retrofit Building Design Code & Code (if applicable): N/A

#### SITE INFORMATION

Site Class: D	Basis:	Inferred
Geologic Hazards:		
Fault Rupture: No	Basis:	CGS Earthquake Hazards Zone Application
Liquefaction: Yes	Basis:	CGS Earthquake Hazards Zone Application
Landslide: No	Basis:	CGS Earthquake Hazards Zone Application

#### ATTACHMENT

Original Structural Drawings: (Bank of America, Ocean Park Venice Office, G.D. Meyers & Associates, 1978, N/A)

Seismic Evaluation: (VENICE DENT - CAAN #4327, KPFF, 4/15/2021, ASCE 41-17 Tier 1) Retrofit Structural Drawings: (N/A, N/A, N/A, N/A)



#### **CERTIFICATION & PRESUMPTIVE RATING VERIFICATION STATEMENT**

I, Mark Hershberg, a California-licensed structural engineer, am responsible for the completion of this certificate, and I have no ownership interest in the property identified above. My scope of review to support the completion of this certificate included both of the following ("No" responses must include an explanation):

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- a) the review of structural drawings indicating that they are as-built or record drawings, or that they otherwise are the basis for the construction of the building: ☑ Yes □ No
- b) visiting the building to verify the observable existing conditions are reasonably consistent with those shown on the structural drawings: □ Yes ☑ No
  Due to Covid-19 protocols, building was observed from exterior only.

Based on my review, I have verified that the UCOP Seismic Performance Level (SPL) is presumptively permitted by the following UC Seismic Program Guidebook provision (choose one of the following):

□ 1) Contract documents indicate that the original design and construction of the aforementioned building is in accordance with the benchmark design code year (or later) building code seismic design provisions for UBC or IBC listed in Table 1 below.

☑ 2) The existing SPL rating is based on an acceptable basis of seismic evaluation completed in 2006 or later.

□ 3) Contract documents indicate that a comprehensive<sup>1</sup> building seismic retrofit design was fullyconstructed with an engineered design based on the 1997 UBC/1998 *or later* CBC, and (choose one of the following):

□ the retrofit project was completed by the UC campus. Further, the design was based on ground motion parameters, at a minimum, corresponding to BSE-1E (or BSE-R) and BSE-2E (or BSE-C) as defined in ASCE 41, or the full design basis ground motion required in the 1997 UBC/1998 CBC *or later* for EXISTING buildings, and is presumptively assigned an SPL rating of IV.

□ the retrofit project was completed by the UC campus. Further, the design was based on ground motion parameters, at a minimum, corresponding to BSE-1 (or BSE-1N) and BSE-2 (or BSE-2N) as defined in ASCE 41, or the full design basis ground motion required in the 1997 UBC/1998 *or later* CBC for NEW buildings, and is presumptively assigned an SPL rating of III.

□ the retrofit project was not completed by the UC campus following UC policies, and is presumptively assigned an SPL rating of IV.

<sup>&</sup>lt;sup>1</sup> A comprehensive retrofit addresses the entire building structural system as indicated by the associated seismic evaluation, as opposed to addressing selective portions of the structural system.

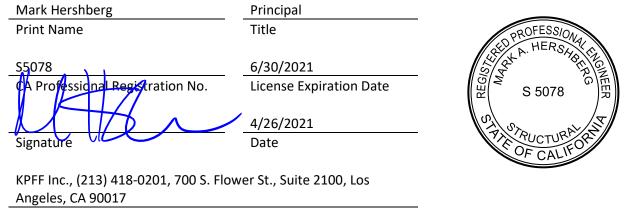
Campus: UCLA Building Name: Venice Dentistry CAAN ID: 4327 Auxiliary Building ID:



Date: Apr 27, 2021

#### **CERTIFICATION SIGNATURE**

AFFIX SEAL HERE



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OF

Firm Name, Phone Number, and Address

Campus: UCLA Building Name: Venice Dentistry CAAN ID: 4327 Auxiliary Building ID:



# UNIVERSITY OF CALIFORNIA

#### Table 1: Benchmark Building Codes and Standards

	Building Seismic Design Provisions	
Building Type <sup>a,b</sup>	UBC	IBC
Wood frame, wood shear panels (Types W1 and W2)	1976	2000
Wood frame, wood shear panels (Type W1a)	1976	2000
Steel moment-resisting frame (Types S1 and S1a)	1997	2000
Steel concentrically braced frame (Types S2 and S2a)	1997	2000
Steel eccentrically braced frame (Types S2 and S2a)	1988 <sup>g</sup>	2000
Buckling-restrained braced frame (Types S2 and S2a)	f	2006
Metal building frames (Type S3)	f	2000
Steel frame with concrete shear walls (Type S4)	1994	2000
Steel frame with URM infill (Types S5 and S5a)	f	2000
Steel plate shear wall (Type S6)	f	2006
Cold-formed steel light-frame construction—shear wall system (Type CFS1)	1997 <sup><i>h</i></sup>	2000
Cold-formed steel light-frame construction—strap-braced wall system (Type CFS2)	f	2003
Reinforced concrete moment-resisting frame (Type C1) <sup>i</sup>	1994	2000
Reinforced concrete shear walls (Types C2 and C2a)	1994	2000
Concrete frame with URM infill (Types C3 and C3a)	f	f
Tilt-up concrete (Types PC1 and PC1a)	1997	2000
Precast concrete frame (Types PC2 and PC2a)	f	2000
Reinforced masonry (Type RM1)	1997	2000
Reinforced masonry (Type RM2)	1994	2000
Unreinforced masonry (Type URM)	f	f
Unreinforced masonry (Type URMa)	f	f
Seismic isolation or passive dissipation	1991	2000

Note: This table has been adapted from ASCE 41-17 Table 3-2. Benchmark Building Codes and Standards for Life Safety Structural Performed at BSE-1E. Note: UBC = Uniform Building Code. IBC = International Building Code.

<sup>a</sup> Building type refers to one of the common building types defined in Table 3-1 of ASCE 41-17.

<sup>b</sup> Buildings on hillside sites shall not be considered Benchmark Buildings.

<sup>c</sup> not used

<sup>d</sup> not used

<sup>e</sup> not used

<sup>f</sup> No benchmark year; buildings shall be evaluated in accordance with Section III.J.

<sup>g</sup> Steel eccentrically braced frames with links adjacent to columns shall comply with the 1994 UBC Emergency Provisions, published September/October 1994, or subsequent requirements.

<sup>h</sup> Cold-formed steel shear walls with wood structural panels only.

<sup>1</sup> Flat slab concrete moment frames shall not be considered Benchmark Buildings.



# UCLA – Venice Dentistry

DATE: 4/27/2021 ASCE 41-17 Tier 1 Seismic Evaluation Minimum Building Report Information

## **BUILDING DATA**

Campus: UCLA Building Name: Venice Dentistry CAAN ID: 4327 Auxiliary Building ID: Address: 323 South Lincoln Blvd, Los Angeles, CA, 90291 Site location coordinates: Latitude 34.00096759 Longitudinal -118.4671674



## ASCE 41-17 Model Building Type:

- a. Longitudinal Direction: W2: Wood frame, wood shear panels
- b. Transverse Direction: W2: Wood frame, wood shear panels

Site-specific Ground Motion Study? No

Seismic Design Acceleration Parameters of Interest:

- a. For BSE-1E  $S_{XS}=0.873g$  and  $S_{X1}=0.494g$
- b. For BSE-2E  $S_{XS}$ =1.735g and  $S_{X1}$ =0.899g

Estimated Fundamental Period (seconds)

- a. Longitudinal: 0.15s
- b. Transverse: 0.15s

Gross Square Footage: 9,443 Number of stories *above* grade: 1 Number of basement stories below grade: 0

Year Original Building was Constructed: 1978 Original Building Design Code & Year: UBC-1973 Retrofit Building Design Code & Code (if applicable): N/A

## SITE INFORMATION

Site Class: D	Basis:	Inferred
Geologic Hazards:		
Fault Rupture: No	Basis:	CGS Earthquake Hazards Zone Application
Liquefaction: Potentially	Basis:	CGS Earthquake Hazards Zone Application
Landslide: No	Basis:	CGS Earthquake Hazards Zone Application

## UCOP SEISMIC PERFORMANCE RATING (OR "RATING"): V

## "BALLPARK" RETROFIT COST (if applicable)

$\boxtimes$	Minor (<\$50/sf)
	Moderate (~\$50-\$200/sf)
	Major (>\$200/sf)

# SUMMARY TIER 1 SEISMIC EVALUATION STRUCTURAL NON-COMPLIANCES/FINDINGS SIGNIFICANTLY AFFECTING RATING DETERMINATION

Significant Structural Deficiencies, Potentially Affecting Seismic Performance Level Designation:

- $\boxtimes$ Lateral System Stress Check (wall shear, column shear or flexure, or brace axial as applicable)
- Lateral System Detailing (reinforcement ratio, confinement, aspect ratio, etc)
- Load Path
- Adjacent Buildings
- Weak Story
- Soft Story
- Geometry (vertical irregularities)
- Torsion
- Mass Vertical Irregularity
- **Cripple Walls**
- Wood Sills (bolting)
- $\boxtimes$ Diaphragm Continuity
- Openings at Shear Walls (concrete or masonry)
- Liquefaction

- Slope Failure
- Surface Fault Rupture
- Masonry or Concrete Wall Anchorage at Diaphragm
- URM wall height to thickness ratio
- **URM** Parapets or Cornices
- URM Chimney
- Heavy Partitions Braced by Ceilings
- Appendages

# POTENTIAL FALLING HAZARDS

- Heavy ceilings, features or ornamentation above large lecture halls, auditoriums, lobbies or other areas where large numbers of people congregate.
- Heavy masonry or stone veneer above exit ways.
- Unbraced masonry parapets, cornices or other ornamentation above exit ways.
- Unrestrained hazardous materials storage.
- Masonry chimneys.
- Unrestrained natural gas-fueled equipment such as water heaters, boilers, emergency generators, etc.
- $\boxtimes$ None of the above.

Due to current COVID-19 protocols, we did not verify in field that as-built documentation match current conditions or perform any condition assessment of the existing structure to identify falling hazards as required by the UCOP SSP.

# **BRIEF DESCRIPTION OF ANTICIPATED FAILURE MECHANISM**

The primary failure mechanism anticipated at this structure is failure of the wood shear walls, which are overstressed by a factor of over 2 based on the prescribed Tier 1 checks. In addition to this, there are diaphragm continuity issues at the intersection between the typical roof and the mezzanine, which are set at different elevations. While there appears to be a defined load path at this location that intends to drag load back into the primary lateral force resisting system, there are concerns associated with discontinuous chord members that run perpendicular to the step in the diaphragm at each side of the structure.

## COMMENTS AND RECOMMENDATIONS

It is recommended that a Tier 2 evaluation be performed. A Tier 2 evaluation will provide more information related to the potential wall stress and diaphragm continuity issues that were observed in the Tier 1 evaluation.

## Appendices

- A. ASCE 41-17 Tier 1 Checklists
- B. Quick Check Calculations